Since its inception over a decade ago, HFOV has become an increasingly utilised and effective strategy for the treatment of acute lung injury and acute respiratory distress syndrome. During HFOV, the lungs are recruited and stabilised to avoid the cyclic stretch and shear exerted on the alveoli which occur during conventional ventilation by repeated alveolar collapse and re-expansion. Patients with deteriorating gas exchange despite increasing ventilatory settings can be successfully managed with HFOV as it provides significant lung protection. However, as with any mode of ventilation, management strategies must be designed to minimise (or eliminate) ventilator-induced lung injury based on a patient’s pathophysiology.

Mechanical ventilatory strategies have evolved dramatically over the past decade. The deleterious effects of mechanical ventilation have been widely studied and are universally recognised. When high peak airway pressures, elevated mean airway pressures, excessive FiO2, and/or large tidal volumes...
are necessary to maintain adequate gas exchange, patients are at risk of developing ventilator-associated lung injury. High-frequency ventilation was first introduced in the late 1970s as an alternative method of mechanical ventilation designed specifically to reduce the complications associated with conventional mechanical ventilation.

High-frequency ventilation is defined as a delivered tidal volume that is less than anatomical dead space and delivered at a high frequency rate (> 120 breaths per minute for adults, > 150 breaths per minute for infants and children). This relationship between dead space and ventilation was discussed as early as 1915 when Henderson and colleagues theorised that gas exchange sufficient to support life could be achieved even at tidal volumes considerably less than dead space. However, it was not until the 1970s that interest in a clinical application of high-frequency ventilation emerged. Studies during the 1970s clearly demonstrated in animal models of acute lung injury that adequate alveolar ventilation could be achieved with tidal breaths smaller than anatomical dead space and accelerated breathing frequencies. When ventilating with these extremely small tidal volumes, peak airway pressures are dramatically reduced leading to the belief that high-frequency ventilatory approaches minimise the adverse effects of volutrauma, barotrauma, and stretch injury associated with conventional ventilation.

The two most common forms of high-frequency ventilation are high-frequency jet ventilation (HFJV) and high-frequency oscillatory ventilation (HFOV). HFJV is most commonly performed via the Life Pulse ventilator (Bunnell Inc., Salt Lake City, Utah, USA), which delivers pulses of gas at a high velocity through an orifice at a frequency of 240 - 660 breaths per minute. The small high-velocity breaths and fast rates coupled with passive exhalation provide an effective means for carbon dioxide elimination at reduced peak airway pressures. A key concept of high-frequency ventilation (both oscillation and jet) is that the swing from maximal to minimal airway pressure is attenuated as gas flow progresses from the ventilator to the alveoli (Fig. 1). This may also be described as an attenuation of the peak-to-trough swing across the mean airway pressure. HFOV is an attractive alternative to conventional mechanical ventilation for the respiratory management of a wide range of critically ill patients with acute lung injury.

Theory of gas exchange during HFOV

While the gas exchange mechanisms during conventional mechanical ventilation are convection ventilation or ‘bulk flow’, gas exchange during HFOV is enhanced by other mechanisms. Even with the small tidal volumes of HFOV, direct alveolar ventilation may occur to short path length units that branch from the primary airways. However, this only accounts for a small component of the gas exchange that occurs during HFOV.

Molecular diffusion is speculated to be a major contributor to gas exchange during oscillatory ventilation. Molecular diffusion describes gas exchange across the alveolar-capillary membrane and contributes to the transport of both oxygen and carbon dioxide in the gas phase near the membrane. In 1984, Slutsky and colleagues theorised that the gas exchange mechanism during HFOV was caused by the coupled effects of convection and molecular diffusion. It is speculated that this is due to an increase in turbulence of the molecules during high-frequency oscillation. In that same year, Chang and colleagues determined that a convective mechanism may predominate with the increased tidal volume at lower ventilatory rates, while a diffusive mechanism may...
predominate with the decreased tidal volume at higher frequencies.

Taylor dispersion is also proposed as a significant contributor to gas exchange. Taylor dispersion occurs when a high velocity of gas travels down the centre of a tube, leaving the molecules on the periphery unmoved. When the high-velocity flow stops, gas molecules then diffuse evenly along the tube (Fig. 2). A variation of this theory describes an asymmetrical velocity profile. During inspiration, the high-frequency pulse creates a 'bullet'-shaped profile with the central molecules moving further down the airway than those molecules found on the periphery of the airway (i.e. 'two steps forward' approach) (Fig. 3).

Still another theory was proposed by Lehr et al., who attributed effective gas exchange during HFOV to the Pendeluft effect. At high frequencies, gas distribution becomes strongly influenced by time-constant inequalities. Gas from fast units (i.e. short time constants) will empty into the slow units (i.e. long time constants) (Fig. 4).

It is likely that a combination of these mechanisms (rather than a single mechanism) is responsible for the effectiveness of gas exchange during HFOV. It is possible that all of these proposed mechanisms coupled with cardiogenic mixing, in which the heartbeat adds to the gas mixing, contribute to the effective gas exchange abilities of HFOV.

**HFOV specifications**

Currently, the most commonly used devices to perform HFOV are the SensorMedics 3100A and 3100B ventilators (Viasys Healthcare, Yorba Linda, California, USA). These ventilators are electronically controlled piston-diaphragm high-frequency ventilators. The 3100A is designed to ventilate all patients regardless of weight; however, carbon dioxide elimination may be ineffective for some 'larger' patients. The 3100B oscillator is FDA approved only for patients weighing more than 35 kilograms.

The 3100A utilises bias flow rates of 0 to 40 l/min and is capable of delivering mean airway pressures between 3 and 45 cm H$_2$O. The 3100B has an increased bias flow ability (0 - 60 l/min) and can deliver higher mean airway pressures (3 - 55 cm H$_2$O). Inspiratory times range between 33% and 50% for the 3100A and between 30% and 50% for the 3100B. Both oscillators utilise similar frequency (3 - 15 hertz) and amplitude (8 - 90 cm H$_2$O) ranges; however, the lower bias flow ranges of the 3100A often make it difficult to achieve the higher mean airway pressures and larger amplitude requirements for 'larger' patients.

**Physiology of gas exchange**

During HFOV, oxygenation and ventilation are decoupled. Oxygenation is primarily a function of FiO$_2$ and Paw. Mean airway pressure is used to inflate the lung and optimise the alveolar surface area for gas exchange (i.e. Paw equals lung volume). Paw during HFOV is created by a continuous bias flow of gas past a resistance (inflation) of a balloon on the mean airway pressure valve. Therefore, the Paw is changed by adjusting the bias flow or the inflation of the balloon control valve (Paw adjust knob). Simply stated, Paw during HFOV is a clinician set value, not a byproduct of other variables. In fact, the Paw of the oscillator...
without the piston moving is a continuous positive airway pressure (CPAP) system.

As with conventional ventilation, carbon dioxide elimination during HFOV is achieved by adjusting the minute ventilation. However, during conventional ventilation minute ventilation is defined as tidal volume times frequency (Vt x f), whereas during HFOV, minute ventilation is equal to Vt x f x % Ti. Therefore, changes in tidal volume delivery have the most significant effect on carbon dioxide elimination.

Tidal volume delivery during HFOV is defined as the gas displaced by the movement of the oscillatory piston. The amount of movement is a function of delta P (i.e. amplitude), frequency, and per cent inspiratory time (% Ti). The primary control of carbon dioxide elimination is the delta P. Delta P displayed on the front panel is produced by adjustment of the power setting. The delta P produces a stroke volume (also referred to as amplitude). The amplitude itself is created by the distance that the piston moves resulting in volume displacement and a visible patient ‘chest wiggle’ (i.e. oscillation).

The secondary control of carbon dioxide elimination is the frequency setting. The power controls the force with which the piston moves, and the frequency controls the time allowed (distance) for the piston to move. Therefore, the lower the frequency the greater the volume displaced; and the higher the frequency, the smaller the volume displaced (Fig 5). The % Ti also controls the time for movement of the piston and can therefore assist in carbon dioxide elimination as well. Increasing the % Ti is generally a technique used for ventilating larger patients.

**Clinical indications**

Patients with diffuse alveolar diseases, such as acute respiratory distress syndrome (ARDS), acute lung injury (ALI), bronchiolitis and air leak syndrome, may benefit from the use of HFOV. Most patients who require high ventilatory settings during conventional ventilation could potentially benefit from HFOV. Consider HFOV for patients with oxygen requirements greater than 0.60, peak inspiratory pressures greater than 32 cm H2O, and mean airway pressures in excess of 15 cm H2O. Patients without cyanotic congenital cardiac lesions who have an oxygen index of greater than 13 on two consecutive arterial blood gases within a 6-hour period should also be considered candidates for HFOV.

Careful consideration should be employed when intracranial hypertension is present. The potential benefit of improved gas exchange at lower airway distending pressures should be carefully weighed against the risk of further increasing intracranial pressures.

**Initiation of HFOV**

When preparing patients for conversion to HFOV always consider the underlying pathology and thoroughly review the chest radiographs and arterial blood gases. It is also important to know the most recent mean airway pressure obtained during conventional ventilation. If the patient’s pH is less than 7.25, consider buffering with sodium bicarbonate (NaHCO3) before initiating HFOV. It should be noted that the use of sodium bicarbonate to buffer acidosis in this situation remains controversial. Growing evidence in the literature discourages this practice.

Most patients should have a functional arterial line. Pulse oximetry is absolutely essential. Transcutaneous oxygen and carbon dioxide monitoring is extremely useful. As patient size increases, the reliability of transcutaneous oxygen monitoring decreases. However, with newer technology available transcutaneous carbon dioxide monitoring is a very reliable trend monitor in most patients regardless of size. A central venous line may be helpful. A pulmonary artery catheter is not necessary and, in fact, is rarely utilised for this population of patients.

Sedation is required for most infants, and some may require paralysis. Essentially all paediatric and adult patients require sedation, and most will require paralysis at least initially. However, once the patient has entered the weaning phase, a trial without neuromuscular blockade should be done.

The patient should be suctioned before initiation of HFOV to assure the removal of excess secretions. Since de-recruitment may occur with suctioning, suctioning should be based on the patient’s overall clinical status. Closed suction catheter systems can be used; however, it is essential to completely remove the suction catheter tip from the endotracheal tube (ETT) at the completion of suctioning. When catheters remain in the ETT, the delivered amplitude will be attenuated and a decrease in the ‘chest wiggle factor’ will be seen. Additionally, if a disconnect between the suction adaptor and the ETT occurs, there may be sufficient pressure to prevent the low pressure alarm from sounding. Oximetry and transcutaneous monitoring have the added benefit of notifying the clinician of adverse patient effects secondary to circuit disconnects.
Before transition from conventional to high-frequency ventilation, the clinician should ensure that the patient has adequate intravascular volume and cardiac output. Intravascular volume loading may be required on initiation of HFOV secondary to the associated increase in intrathoracic pressure.30-32 When available, the central venous pressure (CVP) should be monitored to assist in intravascular fluid management. Patients often require a low-dose inotrope infusion to augment cardiac output during the transition to HFOV.

On initiating HFOV, the FiO2 should be set at 1.0. The bias flow should be set at 18 l/min or more for neonatal and paediatric patients. A 30 - 40 l/min bias flow is often required for larger paediatric and adult patients. An adequate bias flow is necessary to assure replenishment of the oxygen supply to the endotracheal tube and for optimal carbon dioxide removal from the circuit. If the bias flow is inadequate, circuit dead space increases and carbon dioxide removal can be impaired. The bias flow should be increased in increments of 5 l/min when carbon elimination is inadequate despite appropriate amplitude and frequency adjustments.

The mean airway pressure on the oscillator should be set at 4 - 8 cm H2O above the level generated on the conventional mechanical ventilator for patients with diffuse alveolar disease.30,31 This increase is required secondary to the pressure attenuation which can occur along the oscillator circuit, endotracheal tube and airways. Additionally, the increased mean airway pressure is intended to augment lung recruitment in patients with acute alveolar injury (i.e. acute lung injury or acute respiratory distress syndrome). The frequency should be set according to the patient’s weight and age (Table I). The % Ti should be set initially at 33% on the 3100A and 30% on the 3100B. The power setting control should be set at 6 and then adjusted to meet the desired amplitude. The power setting needed to provide an adequate amplitude (and chest oscillation) is dependent on the patient’s size, weight and pulmonary compliance.

When titrating the power setting to achieve the optimal amplitude, the clinician should observe the patient for adequate ‘chest wiggle’ and therefore adequate chest oscillation. The amplitude is considered appropriate when the patient has a visible oscillation from the chest to the upper thighs. Transcutaneous carbon dioxide monitoring is also useful for setting the amplitude. In larger patients, the transcutaneous values may not be identical to the arterial blood gas values; however, transcutaneous monitoring can be used successfully for the trending of gas exchange in most patients.

A decrease in chest oscillation is a clinical sign that pulmonary compliance has decreased. If a decrease in chest oscillation is noted, assess the airway to determine if there is an obstruction, then consider endotracheal tube suctioning. A unilateral reduction in chest oscillation indicates that the endotracheal tube may be in the right mainstem bronchus or a pneumothorax may be present. Check the endotracheal tube position and obtain a chest radiograph. Always reassess the chest oscillation following any change in patient position.

Patients with air leak syndrome require a low lung volume strategy even with HFOV. Therefore, a relatively lower mean airway pressure should be used. The Paw setting in unilateral air leak syndrome is dependent on the inflation of the unaffected lung. The clinician should accept less than optimal arterial blood gas values until the air leak resolves. Accept oxygen saturations of 85 - 90% with incremental increases in the FiO2 as needed. Atelectasis is a possibility when ventilating with a low lung volume strategy. Hypercarbia with a pH of 7.25 or greater should be acceptable.33 When adequate oxygenation and ventilation are achieved, decrease the mean airway pressure and amplitude. A higher FiO2 must often be accepted with air leak syndrome to provide for the lowest airway pressures and thus provide optimal lung protection. Once the chest tube air leak has resolved for least 24 hours, gently recruit the collapsed lung and begin weaning.

### HFOV management strategies

Inadequate oxygenation requires adjustment of the mean airway pressure. Paw should be adjusted until optimal lung volume is achieved. Adjustments in Paw should generally be performed in increments of 1 - 2 cm H2O for infants and children and 2 - 3 cm H2O for adult patients. Lung volume is considered optimal when lung expansion is at the 9th thoracic vertebra (T9) on a chest radiograph. It is at this level that there should be a resultant increase in oxygen saturation which will allow for the reduction of FiO2. To optimise lung recruitment, consider a sustained inflation (volume recruitment) manoeuvre. Sustained inflation manoeuvres allow for a more rapid increase in lung volume compared with a gradual increase in the mean airway pressure.34,35 Sustained inflation manoeuvres may be performed while on the HFOV by increasing the Paw by 5 - 8 cm H2O for 30 - 40 seconds while the piston is stopped. At completion of a volume
recruitment manoeuvre, the mean airway pressure should be returned to the previous setting.

When performing a sustained inflation manoeuvre, risks do exist, such as haemodynamic instability and pneumothorax. Always monitor the patient’s haemodynamic status when manipulating the mean airway pressure as perfusion must be matched to ventilation for adequate oxygenation to be achieved. It is also important to note that pulmonary vascular resistance is increased with either atelectasis or pulmonary overdistension. Therefore, the clinician should utilise chest radiographs and pulse oximetry to optimise lung recruitment while guarding against overexpansion. If the chest radiograph demonstrates optimal expansion, the FiO₂ has been maximised and oxygenation remains poor, increasing the % Ti to 50% will raise the distal PAW closer to the proximal values. Thus, increasing the % Ti will increase the effective PAW. It is important to note that increasing the % Ti will also increase the delivered tidal volume.

Managing carbon dioxide elimination is primarily performed by manipulating the power setting control. To reduce the PaCO₂, increase the power setting control (i.e. amplitude) in 3 - 5 cm H₂O increments. Additionally, if the amplitude has been increased by 10 - 20 cm H₂O and there is a clinically inadequate decrease in the PaCO₂, decrease the set frequency. The frequency should be manipulated in increments of 0.5 - 1 Hz. If the initial frequency is too high, unacceptable PaCO₂ levels may result. It is important to note that PaCO₂ may initially climb in large patients before it stabilises and then decreases. Therefore, allow a 5 - 10-minute stabilisation period after each parameter change. Permissive hypercapnia should be acceptable for most patients.

A decrease in chest oscillation (‘chest wiggle’) is a clinical sign that pulmonary compliance has decreased. The assessment of a change in chest oscillation is discussed in more detail under ‘Initiation of HFOV’.

In larger patients with an unacceptable PaCO₂, the % Ti provides an additional means for improving carbon dioxide elimination. While it is recommended that the % Ti be set at 30% when utilising the 3100B and 33% when utilising the 3100A, if the amplitude has been maximised and the frequency has been minimised, increase the inspiratory time towards 50%. Increasing the % Ti will increase the delivered tidal volume and, therefore, should improve ventilation. Additionally, for patients with cuffed endotracheal tubes, minimally deflating the cuff may improve ventilation by allowing for passive exhalation around the endotracheal tube throughout the entire breath cycle (Fig. 6).

**Patient assessment**

Obtain an initial chest radiograph approximately 1 hour after the initiation of HFOV. Then obtain a chest radiograph every 12 hours for the first 24 hours of HFOV. The initial 24 hours, chest radiographs can generally be obtained once daily. While obtaining the chest radiograph, it is not necessary to stop the piston or reposition the head. Do not remove the patient from the oscillator and manually ventilate as this will not provide the information necessary to manage the oscillator as lung expansion will have changed.

Assessment of breath sounds during HFOV is difficult and identifying cardiac sounds is nearly impossible. To assess breath sounds it is not necessary to stop the piston. Listen for the intensity and quality of sounds throughout the chest. Breath sounds should be symmetrical. Always take any changes in breath sounds seriously. When a change is noted, stop the piston for further evaluation. When the piston is stopped the patient is on CPAP. Obtain a chest radiograph if there is any concern. When assessing cardiac sounds the piston must be stopped. Listen quickly to the heart sounds and restart the piston.

**Weaning and conversion to conventional mechanical ventilation**

The initial approach to weaning should be a reduction in the most toxic ventilatory parameter(s). Patients with diffuse alveolar disease should begin with a reduction in the FiO₂. Once FiO₂ has been reduced to less than 0.60, begin weaning the mean airway pressure. The Paw should be decreased in increments of 1 - 2 cm H₂O for oxygen saturations greater than approximately 88% while maintaining adequate lung volume. De-recruitment occurs much more slowly than recruitment. In the event that lung volume is lost during the process of weaning, adequate lung volume can be quickly achieved with a sustained inflation manoeuvre followed by an incremental increase in the Paw.
The frequency should be increased in increments of 0.5 - 1 Hz until it is returned to the appropriate rate based on the patient's age and weight. Once the appropriate frequency is achieved, begin weaning the amplitude. The amplitude should be decreased in increments of 3 - 5 cm H₂O using the transcutaneous monitor as a guide. The PEEP should be returned to 30% for 3100B patients and 33% for patients ventilating with the 3100A before conversion to conventional ventilation.

Once the lung process has stabilized, the oscillatory support has been minimised and the arterial blood gases have improved, consider transition to conventional mechanical ventilation. While every support has been minimised and the arterial blood gases have improved, consider conversion to conventional ventilation.